

Process and Apparatus for Irradiating Fluids

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The present invention relates to a process and an apparatus for subjecting fluids to irradiation by high intensity ultrasound.

If a liquid is subjected to a high ultrasonic intensity, that is to say an intensity greater than about 0.3 W/cm^2 at a frequency typically in the range 10 kHz to 100 kHz, then there is a significant deposition of energy into the liquid through attenuation and non-linear effects. This may lead to physical changes (for example streaming, mixing, or emulsification) or to chemical changes, and the present invention is principally concerned with the latter, which may be referred to as sonochemistry. The most significant sonochemical effects are usually associated with cavitation in the liquid, especially transient vaporous cavitation, which typically only occurs at an ultrasonic intensity above a threshold which is typically above 0.3 W/cm^2 and is different for different liquids.

An apparatus for subjecting a liquid to a very high intensity is described in GB 2 243 092 B (UKAEA), in which a transducer is attached to one end of a tapered resonant coupler, the coupler having a nodal flange; this flange is attached to a sleeve projecting from the wall of a pipe containing the liquid, and the space around the sides and end of the coupler within the sleeve is filled with a coupling liquid such as olive oil. The use of such a nodal flange mounting enables a transducer of higher power to be used, but the apparatus is somewhat complex. It has also been suggested, for example in US 4 433 916

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(Hall), to attach a plurality of acoustic transducers directly to the wall of a cylindrical vessel containing a fluid, with a specified phase difference between the acoustic signals applied to adjacent transducers.

- 5 Similarly, US 4 369 100 (Sawyer) describes attaching ultrasonic transducers to the outer wall of an annular duct so that both the inner and outer walls are set in resonance. And US 2 578 505 (Carlin) also describes a pipe with several transducers attached to the surface
10 arranged in one or more circumferential rings.

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- According to the present invention there is provided an apparatus for subjecting a fluid to irradiation by high intensity ultrasound, the apparatus comprising a
15 generally cylindrical vessel, and a multiplicity of ultrasonic transducers attached to a wall of the vessel in an array that extends both circumferentially and longitudinally so as to radiate ultrasonic waves into a fluid in the vessel, the vessel being large enough that
20 each transducer radiates into fluid at least 0.1 m thick, each transducer being connected to a signal generator arranged so that the transducer radiates no more than 3 W/cm^2 , the transducers being sufficiently close to each other, and the number of transducers being sufficiently
25 high, that the power dissipation within the vessel is at least 25 W/litre but no more than 150 W/litre.

- The values of power given here are those of the electrical power delivered to the transducer or the
30 transducers, as this is relatively easy to determine. There will inevitably be losses in converting electrical to acoustic power, and in transmitting the acoustic power

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from the transducer into the fluid within the vessel, but these are difficult to assess accurately. The transducer

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typically is at least 90% efficient in converting electrical to acoustic power.

The power radiated by each transducer may for
5 example be in the range $1-2 \text{ W/cm}^2$. This is a similar
power intensity to that used in ultrasonic cleaning
baths, and is above the threshold required to achieve
cavitation. The resonant ultrasonic coupler with a nodal
flange (as described in GB 2 243 092 B) can achieve
10 significantly higher power intensities, for example
radiating more than 10 W/cm^2 , but the lower intensity
ultrasound generated by the present invention can
propagate much further through a liquid, and the stresses
in the transducers are much less.

15 The thickness of fluid into which each transducer
radiates, that is the width or diameter of the vessel, is
preferably no more than 1.2 m, and in a preferred
embodiment the vessel is cylindrical of diameter in the
20 range 0.2 to 0.6 m, such as 0.3 m.

Preferably the number of transducers, the power of
the transducers, and the volume of the vessel are such
that the power density is between 40 and 80 W/litre, more
25 preferably between 60 and 70 W/litre. Although this does
not produce such high power densities as can be achieved
with an irradiator as described in GB 2 243 092 (UKAEA),
it enables a larger volume to be irradiated and with
greater uniformity, at sufficient intensity to cause
30 cavitation; this is partly because very high cavitation
levels near the vessel wall can have the effect of
shielding parts of the fluid further from the wall.

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In a preferred embodiment the vessel is double walled, the transducers being attached to the outer wall, the fluid to be treated being enclosed within the inner wall, and the space between the two walls being filled by
5 a low attenuation buffer liquid whose cavitation threshold is above that of the liquid to be treated.

The width of the gap between the two walls is desirably equal to a quarter wavelength in the coupling
10 liquid (which for a frequency of 20 kHz would be about 18 mm), or an odd-numbered multiple of that distance, to optimise the matching of impedance.

In one embodiment some of the transducers are
15 energized at one frequency and other transducers at a different frequency, for example at 20 kHz and at 40 kHz.

This can be very effective at causing cavitation and energy deposition within a fluid.

The invention will now be further and more particularly described, by way of example only, and with reference to the accompanying drawings in which:

Figure 1 shows a longitudinal sectional view through an
25 irradiator apparatus;

Figure 2 shows a longitudinal sectional view through an alternative irradiator apparatus; and

Figure 3 shows a sectional view on the line 3-3 of figure 2.

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Referring to figure 1 an irradiator 10 incorporates a stainless-steel duct 12 of internal diameter 0.31 m and of wall thickness 2 mm. To the outside of the wall are attached sixty transducer modules 14 closely packed in a square array. Each transducer module 14 comprises a 50 W piezoelectric transducer 16 which resonates at 20 kHz, attached to a conically flared titanium coupling block 18 by which it is connected to the wall, the wider end of each block being of diameter 63 mm. The transducers 10 modules 14 are arranged in five circumferential rings each of twelve modules 14, the centres of the coupling blocks 18 being on a square pitch of 82 mm. The irradiator 10 also incorporates five signal generators 20 (only one is shown) each of which drives all the 15 transducers 16 in a ring. All the transducers 16 are activated at 20 kHz.

In use of the irradiator 10, a liquid is caused to flow through the duct 12 and each transducer 16 20 activated. Each transducer 16 radiates 50 watts over a circle of diameter 63 mm, that is an intensity of 1.6 W/cm². The energy from all the transducers 16 is dissipated over the cylindrical volume of the duct 12, that is to say over a volume of about 31 litres (that is 25 the volume enclosed by the array of transducer modules 14), so the power density is about 97 W/litre, or about 80 W/litre if the ultrasonic irradiation is also effective 40 mm beyond each end of the array of transducer modules 14.

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In one modification, three of the rings of transducers 16 are as described above, while the other two rings resonate at 40 kHz and are driven at that

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frequency (the rings being of alternate frequency along the duct 12). The power intensity and power density are as described earlier, but the fluid is consequently exposed simultaneously to two different frequencies
5 generating cavitation. This can produce more effective sonochemical results.

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10 Referring now to figures 2 and 3 there is shown an alternative irradiator 30 which has many features in common with that of figure 1. The irradiator 30 includes a generally cylindrical duct 32 of polytetrafluoro-ethylene (PTFE) of internal diameter 0.31 m and of wall thickness 3 mm, which tapers at each end down to an internal diameter of 0.10 m and a wall thickness of 6 mm
15 provided with a flange 33 for connection to other process ducts (not shown), and has a sealed joint 34 for inspection or cleaning purposes. Around the outside of the duct 32 is a concentric stainless-steel steel tube 35 of wall thickness 1 mm and of external diameter 0.354 m,
20 such that there is a gap 36 of width 18 mm between the duct 32 and the tube 35. Sixty transducer modules 14 are attached to the outer surface of the tube 35 in a rectangular array forming five rings of twelve, the spacing between the centres of the coupling blocks 18
25 being 82 mm parallel to the longitudinal axis of the tube 35 and 92.7 mm circumferentially. The array of transducers 14 is enclosed by an acoustic shield 38. A coupling liquid such as olive oil 40 is used to fill the gap 36 and is re-circulated from a reservoir 42 by a pump
30 44. This coupling liquid has a higher threshold for cavitation than water, and has an impedance which is between that of the titanium coupling block 18 and that of the fluid within the duct 32 (typically mainly water,

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Sub B3 or an industrial solvent); at a frequency of 20 kHz the wavelength of the sound in this oil is 72 mm, so that the gap 36 is of width equal to a quarter of the wavelength.

Sub B4 5 In use of the irradiator 30, a liquid is caused to flow through the duct 32 and each transducer 16 is activated by a power supply (not shown) at 20 kHz. The dissipated power intensity and power density are as described in relation to figure 1. The impedance
10 matching provided by the oil in the gap 36 allows more of the applied power to enter the fluid within the duct 32 while reducing erosion at the inner, irradiating, surface of the tube 35.

15 It will be appreciated that the power intensity in the irradiator 30 may be increased by increasing the numbers of transducer modules 14 in each ring. For example there might be sixteen transducer modules 14 in each ring, if the coupling blocks 18 were arranged on a
20 circumferential spacing of 69.5 mm. This would increase both the power density and the power intensity by 33 percent. It will also be appreciated that the duct 32 can be of any material suited to the liquid being processed, and that it may form part of a pressure
25 vessel. It will also be appreciated that the duct 12 or 32 need not be cylindrical but might for example be of square cross-section.

Furthermore the ultrasonic frequencies or
30 frequencies might be different from those described above, and might be as high as 140 kHz or even 200 kHz, as such high frequencies tend to reduce the risk of cavitation erosion.

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